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# Computational Modelling of a Caged Methyl Cation: Structure, Energetics and Vibrational Analysis

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**Table S1.** Z-matrix template for TS cage complexes.

C						
X	1	c_1				
X	2	c_1	1	c_90		
H	1	v_CH	2	c_90	3	c_0
H	1	v_CH	2	c_90	3	c_120
H	1	v_CH	2	c_90	3	-c_120
O	1	c_Rax	4	c_90	3	c_0
X	7	c_1	1	c_90	4	c_0
X	7	c_1	8	c_90	1	c_180
H	7	v_HOax	9	v_Aax	8	c_90
H	7	v_HOax	9	v_Aax	8	-c_90
O	1	c_Rax	4	c_90	3	c_180
X	12	c_1	1	c_90	4	c_0
X	12	c_1	13	c_90	1	c_180
H	12	v_HOax	14	v_Aax	13	c_90
H	12	v_HOax	14	v_Aax	13	-c_90
O	1	c_Req	2	c_90	3	c_0
X	17	c_1	1	c_90	2	c_0
X	17	c_1	18	c_90	1	c_180
H	17	v_HOeq	19	v_Aeq	18	c_90
H	17	v_HOeq	19	v_Aeq	18	-c_90
O	1	c_Req	2	c_90	3	c_120
X	22	c_1	1	c_90	2	c_0
X	22	c_1	23	c_90	1	c_180
H	22	v_HOeq	24	v_Aeq	23	c_90
H	22	v_HOeq	24	v_Aeq	23	-c_90
O	1	c_Req	2	c_90	3	-c_120
X	27	c_1	1	c_90	2	c_0
X	27	c_1	28	c_90	1	c_180
H	27	v_HOeq	29	v_Aeq	28	c_90
H	27	v_HOeq	29	v_Aeq	28	-c_90

Variables:

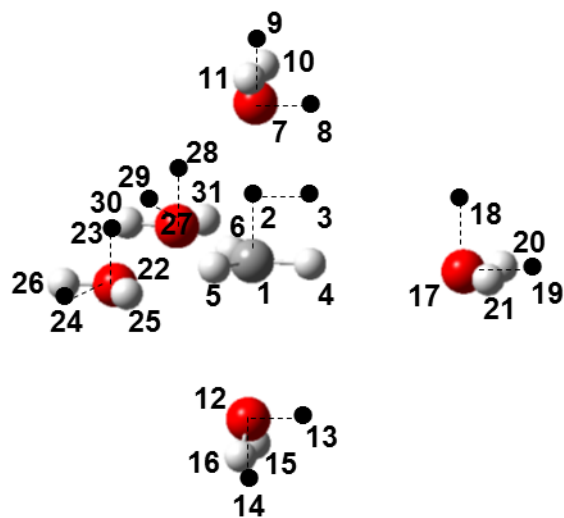
v_CH	1.1014
v_HOax	0.9664
v_Aax	55.0
v_HOeq	0.9656
v_Aeq	54.74

Constants:

c_Rax	2.04
c_Req	3.0
c_0	0.0
c_1	1.0
c_90	90.0
c_120	120.0
c_180	180.0

! this is  $r_{ax}$  in the paper

! this is  $r_{eq}$  in the paper



**Table S2.** B3LYP/aug-cc-pVDZ optimised parameters for cage transition structures.

Rax / Å	Req / Å	CH / Å	HOax / Å	Aax / °	HOeq / Å	Aeq / °
2.04	3.0	1.08499	0.96469	54.6395	0.96596	52.277
	3.05	1.08591	0.96474	54.6675	0.96587	52.2825
	3.10	1.08664	0.96480	54.692	0.96579	52.287
	3.15	1.08719	0.96486	54.7135	0.96572	52.2915
	3.25	1.08790	0.96499	54.7475	0.96563	52.2985
	3.35	1.08220	0.96510	54.772	0.96556	52.302
	3.5	1.08817	0.96528	54.7945	0.96552	52.300
	3.75	1.08750	0.96554	54.8060	0.96551	52.2795
	4.0	1.08667	0.96576	54.8000	0.96553	52.251
2.525	5.0	1.08502	0.96633	54.7275	0.96545	52.193
	3.0	1.09642	0.96467	53.7425	0.96575	52.4315
	3.5	1.09693	0.96498	53.9960	0.96542	52.3712
	3.75	1.09561	0.96515	54.0535	0.96544	52.3275
	4.0	1.09436	0.96530	54.0862	0.96547	52.2835
3.0	5.0	1.09205	0.96572	54.1055	0.96544	52.2005
	3.0	1.10304	0.96505	52.9624	0.96574	52.5279
	3.5	1.10206	0.96519	53.1986	0.96541	52.4223
	3.75	1.10038	0.96528	53.2690	0.96543	52.3640
	4.0	1.09890	0.96536	53.3171	0.96546	52.3084
4.0	5.0	1.09623	0.96565	53.3900	0.96544	52.2050
	3.0	1.10865	0.96540	52.268	0.96592	52.600
	3.05	1.10891	0.96540	52.2755	0.96584	52.587
	3.10	1.10896	0.96540	52.2825	0.96577	52.574
	3.15	1.10888	0.96540	52.290	0.96572	52.561
	3.25	1.10841	0.96540	52.304	0.96564	52.5365
	3.35	1.10770	0.96540	52.317	0.96559	52.512
	3.5	1.10647	0.96541	52.335	0.96557	52.4745
	3.75	1.10428	0.96543	52.360	0.96562	52.409
	4.0	1.10220	0.96545	52.3745	0.96574	52.3505
5.0	1.09738	0.96549	52.366	0.96623	52.2765	

Continued on next page

5.0	3.0	1.10998	0.96536	52.186	0.96608	52.530
	3.05	1.11018	0.96536	52.188	0.96600	52.587
	3.10	1.11019	0.96536	52.1895	0.96593	52.574
	3.15	1.11005	0.96536	52.191	0.96587	52.562
	3.25	1.10947	0.96536	52.194	0.96579	52.538
	3.35	1.10865	0.96536	52.1965	0.96575	52.515
	3.5	1.10722	0.96579	52.2005	0.96573	52.479
	3.75	1.10464	0.96378	52.205	0.96583	52.418
	4.0	1.10125	0.96619	52.2705	0.96568	52.346
	5.0	1.09721	0.96538	52.2125	0.96653	52.300

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**Table S3.** Z-matrix template for RS cage complexes.

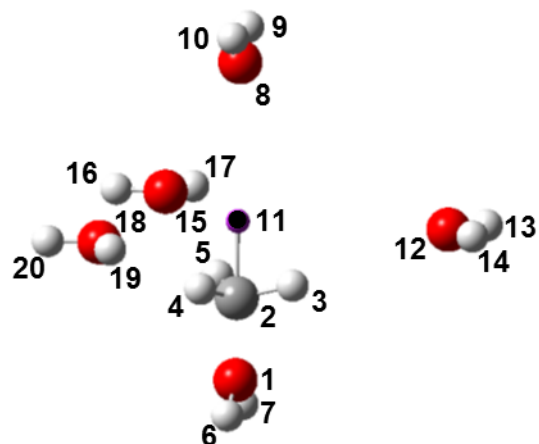
O						
C	1	v_CO				
H	2	v_CH	1	v_OCH		
H	2	v_CH	1	v_OCH	3	c_120
H	2	v_CH	1	v_OCH	3	- c_120
H	1	v_HOax	2	c_Aax	3	c_90
H	1	v_HOax	2	c_Aax	3	- c_90
O	1	c_OO	6	c_Aax	2	c_0
H	8	v_HOax	2	c_Aax	3	c_90
H	8	v_HOax	2	c_Aax	3	- c_90
X	1	c_Rax	6	c_Aax	2	c_0
O	11	c_Req	1	c_90	3	c_0
H	12	c_HOeq	11	c_Aeq	1	c_90
H	12	c_HOeq	11	c_Aeq	1	- c_90
O	11	c_Req	1	c_90	3	c_120
H	15	c_HOeq	11	c_Aeq	1	c_90
H	15	c_HOeq	11	c_Aeq	1	- c_90
O	11	c_Req	1	c_90	3	- c_120
H	18	c_HOeq	11	c_Aeq	1	c_90
H	18	c_HOeq	11	c_Aeq	1	- c_90

Variables:

v_CO	1.56677
v_CH	1.08504
v_OCH	102.0

Constants:

c_OO	4.08	! this is $r_{ax} \times 2$
c_Rax	2.04	! this is $r_{ax}$ in the paper
c_Req	3.0	! this is $r_{eq}$ in the paper
c_HOax	0.96469	
c_Aax	125.361	
c_HOeq	0.96596	
c_Aeq	127.723	
c_0	0.0	
c_90	90.0	
c_120	120.0	



**Table S4.** B3LYP/aug-cc-pVDZ optimised parameters for cage reactant structures.

---

$r_{\text{ax}} / \text{\AA}$	$r_{\text{eq}} / \text{\AA}$	CH / $\text{\AA}$	CO / $\text{\AA}$	HCO <sub>ax</sub> / $^{\circ}$
2.04	3.0	1.08609	1.583	102.249
	3.5	1.09039	1.563	102.825
	3.75	1.09010	1.568	103.174
	4.0	1.08959	1.563	103.428
	5.0	1.08850	1.553	103.953
	$\infty$	1.08818	1.545	104.312
2.525	3.0	1.09287	1.569	103.831
	3.5	1.09420	1.563	104.185
	3.75	1.09359	1.557	104.375
	4.0	1.09289	1.551	104.552
	5.0	1.09166	1.540	104.935
	$\infty$	1.09117	1.533	105.188
3.0	3.0	1.09513	1.565	104.472
	3.5	1.09452	1.554	104.631
	3.75	1.09384	1.547	104.713
	4.0	1.09322	1.543	104.811
	5.0	1.09224	1.532	105.058
	$\infty$	1.09176	1.524	105.278
4.0	3.0	1.09343	1.553	105.079
	3.5	1.09303	1.542	105.0541
	3.75	1.09279	1.538	105.077
	4.0	1.09263	1.535	105.0771
	5.0	1.09222	1.528	105.156
	$\infty$	1.09197	1.519	105.311
5.0	3.0	1.09208	1.537	105.199
	3.5	1.09213	1.532	105.196
	3.75	1.09213	1.531	105.198
	4.0	1.09206	1.530	105.181
	5.0	1.09210	1.525	105.219
	$\infty$	1.09200	1.517	105.322

---



**Table S5.** B3LYP/aug-cc-pVDZ optimised bond lengths (Å) and angles (degrees) for unconstrained RS and TS with  $r_{\text{eq}} = \infty$ .

RS

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OC / Å	C $\cdots$ O / Å	CH / Å	HO <sub>lg</sub> / Å	HO <sub>nuc</sub> / Å	COH <sub>lg</sub> / °	HCO <sub>lg</sub> / °	COH <sub>lg</sub> / °
1.55219	2.67557	1.08941	0.97623	0.96626	113.943	104.854	127.807

---

TS

---

$r_{\text{ax}}$ / Å	CH / Å	HO / Å	COH / °
1.98619	1.08388	0.96995	116.684

---

**Table S6.** B3LYP/aug-cc-pVDZ optimised energies for RS and TS structures (total energies in hartree, relative energies in kJ mol<sup>-1</sup>).

		$r_{\text{eq}}$					
$r_{\text{ax}}$		3.0	3.5	3.75	4.0	5.0	$\infty$
2.04	$E_{\text{RS}}$	-421.86098	-421.86284	-421.85963	-421.85637	-421.84710	-192.49373
	$E_{\text{TS}}$	-421.85431	-421.85515	-421.85132	-421.84755	-421.83715	-192.48296
	$\Delta E^\ddagger$	17.5	20.2	21.8	23.2	26.1	28.3
2.525	$E_{\text{RS}}$	-421.85795	-421.85585	-421.85265	-421.84965	-421.84143	-192.48948
	$E_{\text{TS}}$	-421.83256	-421.82884	-421.82388	-421.81939	-421.80797	-192.45370
	$\Delta E^\ddagger$	66.6	70.9	75.5	79.4	87.8	93.9
3.0	$E_{\text{RS}}$	-421.85239	-421.84793	-421.84511	-421.84261	-421.83569	-192.48528
	$E_{\text{TS}}$	-421.81262	-421.80504	-421.79898	-421.79371	-421.78092	-192.42612
	$\Delta E^\ddagger$	104	113	121	128	144	155
4.0	$E_{\text{RS}}$	-421.83788	-421.83513	-421.83379	-421.83255	-421.82869	-192.48172
	$E_{\text{TS}}$	-421.79497	-421.78306	-421.77555	-421.76925	-421.75556	-192.39894
	$\Delta E^\ddagger$	113	137	153	166	192	217
5.0	$E_{\text{RS}}$	-421.82682	-421.82647	-421.82614	-421.82577	-421.82411	-192.48027
	$E_{\text{TS}}$	-421.78945	-421.77622	-421.76826	-421.76244	-421.74783	-192.39280
	$\Delta E^\ddagger$	98	132	152	166	200	230
unconstrained							
	$E_{\text{RS}}$	-192.49915					
	$E_{\text{TS}}$	-192.48649					
	$\Delta E^\ddagger$	33.2					

**Table S7.** B3LYP/aug-cc-pVDZ average CH-bond stretching force constants ( $\text{aJ \AA}^{-2}$ ) for RS and TS.

$rO_{\text{ax}}$		$rO_{\text{eq}}$					
		3.0	3.5	3.75	4.0	5.0	$\infty$
2.04	(CH) <sub>RS</sub>	5.763	5.620	5.633	5.654	5.708	5.730
	(CH) <sub>TS</sub>	5.863	5.752	5.779	5.812	5.888	5.926
	$\Delta^\ddagger$	0.100	0.132	0.146	0.158	0.180	0.196
	$\Delta\Delta^\ddagger_{\text{eq}}$	-0.096	-0.064	-0.050	-0.038	-0.016	
2.525	(CH) <sub>RS</sub>	5.528	5.502	5.524	5.549	5.603	5.626
	(CH) <sub>TS</sub>	5.543	5.540	5.590	5.636	5.733	5.779
	$\Delta^\ddagger$	0.015	0.038	0.066	0.087	0.130	0.153
	$\Delta\Delta^\ddagger_{\text{eq}}$	-0.138	-0.115	-0.087	-0.066	-0.023	
3.0	(CH) <sub>RS</sub>	5.467	5.496	5.518	5.540	5.580	5.600
	(CH) <sub>TS</sub>	5.320	5.376	5.440	5.495	5.605	5.654
	$\Delta^\ddagger$	-0.147	-0.120	-0.078	-0.045	0.025	0.054
	$\Delta\Delta^\ddagger_{\text{eq}}$	-0.201	-0.174	-0.132	-0.099	-0.029	
4.0	(CH) <sub>RS</sub>	5.547	5.560	5.566	5.571	5.583	5.589
	(CH) <sub>TS</sub>	5.121	5.218	5.297	5.369	5.544	5.578
	$\Delta^\ddagger$	-0.426	-0.342	-0.269	-0.202	-0.039	-0.011
	$\Delta\Delta^\ddagger_{\text{eq}}$	-0.415	-0.331	-0.258	-0.191	-0.028	
5.0	(CH) <sub>RS</sub>	5.629	5.608	5.602	5.600	5.590	5.587
	(CH) <sub>TS</sub>	5.071	5.184	5.275	5.388	5.541	5.597
	$\Delta^\ddagger$	-0.558	-0.424	-0.327	-0.212	-0.049	0.010
	$\Delta\Delta^\ddagger_{\text{eq}}$	-0.568	-0.434	-0.337	-0.222	-0.059	

**Table S8.** B3LYP/aug-cc-pVDZ unscaled harmonic frequencies (as wavenumbers,  $\text{cm}^{-1}$ ) for internal vibrational modes of methyl cation in the centre a constrained cage (TS geometry). Values for CH stretching and in-plane bending (IP) are averages. Values shown in bold type are produced from the full  $57 \times 57$  Hessian. Values shown in regular type are produced by eliminating all elements of the full  $57 \times 57$  Hessian except for the  $12 \times 12$  block corresponding to  $\text{Me}^+$  alone but are identical to those from the full Hessian. Values in *italic* type result from projecting out the translational and rotational degrees of freedom from the  $12 \times 12$  Hessian to obtain six pure vibrational modes for the internal degrees of freedom.

mode	$r_{\text{ax}} / \text{\AA}$	$r_{\text{eq}} / \text{\AA}$					
		3.0	3.5	3.75	4.0	5.0	$\infty$
$\langle \text{CH} \rangle$	2.04	<b>3245</b>	<b>3229</b>	<b>3239</b>	<b>3251</b>	<b>3278</b>	<b>3290</b>
		3245	3229	3239	3251	3278	3290
		<i>3261</i>	<i>3252</i>	<i>3263</i>	<i>3274</i>	<i>3299</i>	<i>3310</i>
	2.525	<b>3130</b>	<b>3159</b>	<b>3179</b>	<b>3196</b>	<b>3231</b>	<b>3247</b>
		3130	3159	3179	3196	3231	3247
		<i>3140</i>	<i>3171</i>	<i>3190</i>	<i>3207</i>	<i>3240</i>	<i>3254</i>
	3	<b>3054</b>	<b>3108</b>	<b>3134</b>	<b>3155</b>	<b>3194</b>	<b>3211</b>
		3054	3108	3134	3155	3194	3211
		<i>3063</i>	<i>3116</i>	<i>3141</i>	<i>3161</i>	<i>3198</i>	<i>3214</i>
	4	<b>2987</b>	<b>3059</b>	<b>3090</b>	<b>3116</b>	<b>3175</b>	<b>3188</b>
		2987	3059	3090	3116	3175	3188
		<i>2997</i>	<i>3066</i>	<i>3096</i>	<i>3118</i>	<i>3164</i>	<i>3188</i>
	5	<b>2969</b>	<b>3047</b>	<b>3083</b>	<b>3121</b>	<b>3174</b>	<b>3193</b>
		2969	3047	3083	3121	3174	3193
		<i>2980</i>	<i>3055</i>	<i>3088</i>	<i>3126</i>	<i>3176</i>	<i>3193</i>
	$\infty$	<b>2956</b>	<b>3040</b>	<b>3080</b>	<b>3113</b>	<b>3177</b>	<b>3148</b>
		2954	3040	3080	3113	3177	3148
		<i>2966</i>	<i>3048</i>	<i>3086</i>	<i>3118</i>	<i>3178</i>	<i>3148</i>
$\langle \text{IP} \rangle$	2.04	<b>1452</b>	<b>1427</b>	<b>1417</b>	<b>1410</b>	<b>1396</b>	<b>1390</b>
		1452	1427	1417	1410	1396	1390
		<i>1453</i>	<i>1433</i>	<i>1427</i>	<i>1423</i>	<i>1417</i>	<i>1414</i>
	2.525	<b>1452</b>	<b>1431</b>	<b>1420</b>	<b>1412</b>	<b>1399</b>	<b>1392</b>
		1452	1431	1420	1412	1399	1392
		<i>1437</i>	<i>1418</i>	<i>1412</i>	<i>1408</i>	<i>1403</i>	<i>1400</i>

	3	<b>1462</b>	<b>1432</b>	<b>1420</b>	<b>1412</b>	<b>1399</b>	<b>1391</b>
		1462	1432	1420	1412	1399	1391
		<i>1433</i>	<i>1413</i>	<i>1408</i>	<i>1403</i>	<i>1398</i>	<i>1395</i>
	4	<b>1462</b>	<b>1431</b>	<b>1419</b>	<b>1413</b>	<b>1398</b>	<b>1394</b>
		1462	1431	1419	1413	1398	1394
		<i>1428</i>	<i>1409</i>	<i>1403</i>	<i>1395</i>	<i>1372</i>	<i>1393</i>
	5	<b>1461</b>	<b>1429</b>	<b>1417</b>	<b>1410</b>	<b>1397</b>	<b>1393</b>
		1461	1429	1417	1410	1397	1393
		<i>1426</i>	<i>1407</i>	<i>1401</i>	<i>1399</i>	<i>1394</i>	<i>1392</i>
	∞	<b>1460</b>	<b>1429</b>	<b>1417</b>	<b>1409</b>	<b>1397</b>	<b>1386</b>
		1461	1428	1417	1409	1397	1386
		<i>1425</i>	<i>1406</i>	<i>1401</i>	<i>1397</i>	<i>1394</i>	<i>1386</i>
OP (UM)	2.04	<b>1364</b>	<b>1330</b>	<b>1315</b>	<b>1304</b>	<b>1283</b>	<b>1272</b>
		1360	1324	1309	1298	1274	1263
		<i>810</i>	<i>735</i>	<i>705</i>	<i>681</i>	<i>629</i>	<i>599</i>
	2.525	<b>1387</b>	<b>1340</b>	<b>1321</b>	<b>1307</b>	<b>1279</b>	<b>1265</b>
		1360	1344	1325	1311	1283	1269
		<i>1213</i>	<i>1160</i>	<i>1139</i>	<i>1122</i>	<i>1089</i>	<i>1069</i>
	3	<b>1448</b>	<b>1406</b>	<b>1389</b>	<b>1376</b>	<b>1349</b>	<b>1335</b>
		1449	1407	1390	1377	1351	1338
		<i>1370</i>	<i>1333</i>	<i>1317</i>	<i>1304</i>	<i>1276</i>	<i>1260</i>
	4	<b>1486</b>	<b>1450</b>	<b>1432</b>	<b>1414</b>	<b>1351</b>	<b>1349</b>
		1486	1450	1432	1410	1351	1349
		<i>1454</i>	<i>1432</i>	<i>1419</i>	<i>1402</i>	<i>1341</i>	<i>1339</i>
	5	<b>1493</b>	<b>1453</b>	<b>1431</b>	<b>1387</b>	<b>1338</b>	<b>1313</b>
		1492	1453	1431	1387	1338	1313
		<i>1466</i>	<i>1443</i>	<i>1425</i>	<i>1383</i>	<i>1337</i>	<i>1313</i>
	∞	<b>1497</b>	<b>1453</b>	<b>1425</b>	<b>1397</b>	<b>1322</b>	<b>1429</b>
		1497	1453	1425	1397	1322	1429
		<i>1471</i>	<i>1443</i>	<i>1420</i>	<i>1395</i>	<i>1321</i>	<i>1428</i>

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**Table S9.** B3LYP/aug-cc-pVDZ unscaled harmonic frequencies (as wavenumbers,  $\text{cm}^{-1}$ ) for methyl cation in the centre a constrained cage (TS geometry), as obtained from the reduced Hessian: all elements of the full  $57 \times 57$  Hessian are eliminated except for the  $12 \times 12$  block corresponding to  $\text{Me}^+$  alone.

mode	$r_{\text{ax}} / \text{\AA}$	$r_{\text{eq}} / \text{\AA}$										
		3.0	3.05	3.10	3.15	3.25	3.35	3.5	3.75	4.0	5.0	$\infty$
	2.04											
$T_z$		260i	261i	263i	264i	267i	271i	276i	283i	288i	300i	307i
$T_x$		284	270	258	248	229	214	199	185	183	186	97i
$R_z$		293	303	308	306	294	284	288	240	201	90	44i
$T_y$		341	330	322	318	313	305	271	272	269	272	274
$R_y$		1026	1029	1030	1030	1028	1024	1017	1006	998	983	924
$R_x$		1054	1057	1058	1058	1057	1054	1049	1040	1032	1017	1010
OP		1360	1358	1355	1351	1343	1335	1324	1309	1298	1274	1263
IP'		1441	1439	1436	1433	1428	1423	1415	1405	1398	1384	1379
IP''		1462	1460	1458	1455	1450	1445	1438	1428	1421	1407	1401
CH		3105	3097	3092	3088	3083	3082	3084	3095	3107	3134	3146
CH'		3313	3307	3303	3300	3298	3298	3301	3311	3323	3349	3361
CH''		3316	3309	3305	3302	3298	3298	3302	3312	3324	3350	3363

mode	$r_{ax} / \text{\AA}$	$r_{eq} / \text{\AA}$											
		3.0	3.05	3.10	3.15	3.25	3.35	3.5	3.75	4.0	5.0	$\infty$	
	2.525												
T <sub>z</sub>		207i						211	216i	221i	230i	236i	
T <sub>x</sub>		241						138	120	114	121	146i	
R <sub>z</sub>		372						317	269	223	105	27i	
T <sub>y</sub>		264						176	163	161	167	171	
R <sub>y</sub>		592						594	574	558	530	465	
R <sub>x</sub>		630						627	610	596	570	560	
OP		1360						1344	1325	1311	1283	1269	
IP'		1441						1427	1416	1408	1395	1386	
IP''		1462						1434	1424	1416	1403	1398	
CH		3105						3016	3035	3052	3087	3102	
CH'		3313						3230	3251	3268	3303	3319	
CH''		3316						3231	3252	3269	3304	3319	
	3.0												
T <sub>z</sub>		150i						149i	156i	162i	173i	180i	
T <sub>x</sub>		220						98	74	65	77	174i	
R <sub>z</sub>		411						407	282	234	112	22i	
T <sub>y</sub>		229						121	102	98	107	114	
R <sub>y</sub>		400						335	382	357	309	223	
R <sub>x</sub>		427						432	407	385	343	327	
OP		1449						1407	1390	1377	1351	1338	
IP'		1460						1430	1418	1410	1397	1386	
IP''		1463						1433	1422	1414	1400	1395	
CH		2926						2967	2992	3012	3051	3068	
CH'		3118						3178	3204	3226	3265	3281	
CH''		3119						3178	3205	3227	3266	3283	

mode	$r_{ax} / \text{\AA}$	$r_{eq} / \text{\AA}$										
		3.0	3.05	3.10	3.15	3.25	3.35	3.5	3.75	4.0	5.0	$\infty$
	4.0											
T <sub>z</sub>		41i	20i	21	31	37	35	19	38i	62i	75	96i
T <sub>x</sub>		205	184	166	149	119	93	59	37i	173i	364i	29i
R <sub>z</sub>		440	437	430	422	403	382	349	293	240	104	50
T <sub>y</sub>		207	186	168	152	122	98	67	23	23i	33	65
R <sub>y</sub>		303	319	328	332	332	324	305	263	68	483i	75
R <sub>x</sub>		309	324	334	338	338	331	313	275	236	133	108
OP		1486	1483	1480	1476	1469	1461	1450	1432	1410	1398	1349
IP'		1462	1458	1455	1452	1445	1439	1430	1418	1411	1399	1393
IP''		1462	1459	1456	1452	1446	1439	1431	1419	1414	1351	1395
CH		2863	2864	2868	2873	2885	2899	2918	2945	2967	3027	3041
CH'		3048	3054	3062	3070	3087	3105	3129	3162	3190	3247	3261
CH''		3049	3055	3062	3071	3088	3105	3129	3163	3191	3250	3262
	5.0											
T <sub>z</sub>		56	67	74	78	81	81	77	65	47	22i	44i
T <sub>x</sub>		201	181	162	145	113	88	50	39i	48i	24i	92
R <sub>z</sub>		450	445	439	430	410	388	354	296	241	103	25i
T <sub>y</sub>		202	181	162	146	115	89	52	36i	46i	21i	26
R <sub>y</sub>		306	322	331	336	336	328	309	269	225	109	33
R <sub>x</sub>		306	322	331	336	336	328	310	269	225	112	29
OP		1492	1489	1486	1482	1474	1466	1453	1431	1387	1338	1313
IP'		1461	1457	1454	1451	1444	1437	1429	1417	1410	1397	1393
IP		1461	1458	1454	1451	1444	1437	1429	1417	1410	1397	1395
CH		2845	2847	2851	2857	2870	2884	2904	2934	2972	3027	3048
CH'		3031	3037	3046	3055	3074	3093	3119	3157	3196	3248	3265
CH''		3031	3038	3046	3055	3074	3093	3119	3157	3196	3248	3266



mode	$r_{ax} / \text{\AA}$	$r_{eq} / \text{\AA}$
		$\infty$
	$\infty$	
OP		1428
IP'		1386
IP''		1386
CH		3011
CH'		3217
CH''		3217

**Table S10.** B3LYP/aug-cc-pVDZ unscaled force constants for methyl cation in the centre a constrained cage (TS geometry), as obtained from the reduced Hessian, for OP (/aJ rad<sup>-2</sup>), T<sub>z</sub> (/aJ Å<sup>-2</sup>) and the interaction force constant OP/T<sub>z</sub> between them (aJ rad<sup>-1</sup>Å<sup>-1</sup>).

$r_{\text{ax}} / \text{Å}$	term	$r_{\text{eq}} / \text{Å}$										
		3.0	3.05	3.10	3.15	3.25	3.35	3.5	3.75	4.0	5.0	$\infty$
2.04	OP	0.121	0.120	0.118	0.116	0.111	0.107	0.101	0.093	0.086	0.074	0.067
	T <sub>z</sub>	<i>0.018</i>	<i>0.017</i>	<i>0.017</i>	<i>0.017</i>	<i>0.017</i>	<i>0.017</i>	<i>0.017</i>	<i>0.015</i>	<i>0.015</i>	<i>0.013</i>	<i>0.012</i>
	OP/T <sub>z</sub>	<b>0.122</b>	<b>0.122</b>	<b>0.123</b>	<b>0.123</b>	<b>0.123</b>	<b>0.124</b>	<b>0.124</b>	<b>0.125</b>	<b>0.125</b>	<b>0.126</b>	<b>0.127</b>
2.525	OP	0.279						0.256	0.246	0.238	0.223	0.215
	T <sub>z</sub>	<i>-0.016</i>						<i>-0.018</i>	<i>-0.019</i>	<i>-0.021</i>	<i>-0.023</i>	<i>-0.024</i>
	OP/T <sub>z</sub>	<b>0.061</b>						<b>0.061</b>	<b>0.061</b>	<b>0.061</b>	<b>0.062</b>	<b>0.063</b>
3.0	OP	0.361						0.341	0.332	0.325	0.309	0.301
	T <sub>z</sub>	<i>-0.011</i>						<i>-0.011</i>	<i>-0.013</i>	<i>-0.014</i>	<i>-0.016</i>	<i>-0.017</i>
	OP/T <sub>z</sub>	<b>0.031</b>						<b>0.029</b>	<b>0.029</b>	<b>0.029</b>	<b>0.029</b>	<b>0.030</b>
4.0	OP	0.411	0.410	0.409	0.408	0.405	0.402	0.397	0.388	0.378	0.342	0.341
	T <sub>z</sub>	<i>0.0004</i>	<i>0.00004</i>	<i>0.0005</i>	<i>0.0008</i>	<i>0.0009</i>	<i>0.0008</i>	<i>0.0005</i>	<i>-0.001</i>	<i>-0.002</i>	<i>-0.003</i>	<i>-0.004</i>
	OP/T <sub>z</sub>	<b>0.012</b>	<b>0.011</b>	<b>0.010</b>	<b>0.009</b>	<b>0.008</b>	<b>0.007</b>	<b>0.006</b>	<b>0.005</b>	<b>0.005</b>	<b>0.004</b>	<b>0.005</b>
5.0	OP	0.418	0.418	0.417	0.416	0.412	0.409	0.403	0.391	0.367	0.340	0.327
	T <sub>z</sub>	<i>0.002</i>	<i>0.003</i>	<i>0.003</i>	<i>0.004</i>	<i>0.004</i>	<i>0.004</i>	<i>0.003</i>	<i>0.002</i>	<i>0.001</i>	<i>-0.0003</i>	<i>-0.0009</i>
	OP/T <sub>z</sub>	<b>0.009</b>	<b>0.008</b>	<b>0.007</b>	<b>0.006</b>	<b>0.005</b>	<b>0.004</b>	<b>0.002</b>	<b>0.001</b>	<b>0.001</b>	<b>0.0005</b>	<b>0.0007</b>
$\infty$	OP	0.422						0.404	0.389	0.373	0.332	
	T <sub>z</sub>	<i>0.003</i>						<i>0.005</i>	<i>0.004</i>	<i>0.003</i>	<i>0.001</i>	
	OP/T <sub>z</sub>	<b>0.008</b>						<b>0.001</b>	<b>0.0003</b>	<b>-0.0002</b>	<b>-0.0001</b>	

**Table S11.** B3LYP/aug-cc-pVDZ electrostatic potential (ESP) and atomic polar tensor (APT) charges for cage transition structures.

$r_{ax} / \text{\AA}$	$r_{eq} / \text{\AA}$	ESP			APT		
		$\langle q_H \rangle$	$q_C$	$q_{Me}$	$\langle q_H \rangle$	$q_C$	$q_{Me}$
2.04	3	0.941	-1.723	1.049	0.159	0.721	1.197
	3.05	0.931	-1.724	1.035	0.150	0.741	1.192
	3.1	0.916	-1.729	1.020	0.142	0.760	1.186
	3.15	0.916	-1.740	1.007	0.135	0.776	1.182
	3.25	0.827	-1.511	0.972	0.123	0.805	1.174
	3.35	0.733	-1.258	0.941	0.113	0.829	1.168
	3.5	0.640	-1.012	0.907	0.102	0.856	1.162
	3.75	0.484	-0.583	0.870	0.089	0.887	1.154
	4	0.417	-0.406	0.845	0.082	0.905	1.150
2.525	3	0.299	-0.095	0.802	0.071	0.931	1.145
	3	0.608	-0.782	1.043	0.212	0.523	1.158
	3.5	0.464	-0.448	0.944	0.150	0.666	1.116
	3.75	0.380	-0.232	0.909	0.136	0.698	1.107
	4	0.333	-0.103	0.895	0.128	0.717	1.100
3	5	0.293	0.003	0.849	0.115	0.743	1.089
	3	0.349	-0.019	1.028	0.244	0.414	1.145
	3.5	0.269	0.163	0.971	0.182	0.564	1.110
	3.75	0.238	0.245	0.952	0.168	0.597	1.100
	4	0.223	0.275	0.940	0.158	0.617	1.093
4	5	0.227	0.226	0.909	0.144	0.645	1.077
	3	0.214	0.347	0.989	0.266	0.307	1.106
	3.05	0.206	0.368	0.985	0.257	0.328	1.100
	3.1	0.196	0.392	0.980	0.249	0.348	1.095
	3.15	0.188	0.412	0.977	0.241	0.367	1.091
	3.25	0.174	0.450	0.971	0.228	0.399	1.082
	3.35	0.168	0.465	0.969	0.216	0.427	1.075
	3.5	0.156	0.498	0.965	0.201	0.460	1.063
	3.75	0.146	0.515	0.958	0.177	0.499	1.031
5	4	0.147	0.504	0.946	0.145	0.416	0.851
	5	0.172	0.360	0.876	0.103	0.119	0.428
	3	0.211	0.345	0.979	0.269	0.287	1.095

3.05	0.199	0.369	0.975	0.260	0.309	1.088
3.1	0.192	0.396	0.970	0.251	0.329	1.082
3.15	0.182	0.419	0.966	0.243	0.348	1.076
3.25	0.166	0.462	0.959	0.228	0.381	1.064
3.35	0.158	0.481	0.957	0.214	0.410	1.053
3.5	0.145	0.514	0.951	0.195	0.444	1.030
3.75	0.136	0.529	0.938	0.162	0.474	0.959
4	0.146	0.448	0.887	0.131	0.382	0.776
5	0.161	0.338	0.822	0.113	0.342	0.682

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## Full citation for reference 15

Frisch, M. J.; Trucks, G. W.; Schlegel, H. B.; Scuseria, G. E.; Robb, M. A.; Cheeseman, J. R.; Scalmani, G.; Barone, V.; Mennucci, B.; Petersson, G. A.; Nakatsuji, H.; Caricato, M.; Li, X.; Hratchian, H. P.; Izmaylov, A. F.; Bloino, J.; Zheng, G.; Sonnenberg, J. L.; Hada, M.; Ehara, M.; Toyota, K.; Fukuda, R.; Hasegawa, J.; Ishida, M.; Nakajima, T.; Honda, Y.; Kitao, O.; Nakai, H.; Vreven, T.; Montgomery, J. A., Jr.; Peralta, J. E.; Ogliaro, F.; Bearpark, M.; Heyd, J. J.; Brothers, E.; Kudin, K. N.; Staroverov, V. N.; Kobayashi, R.; Normand, J.; Raghavachari, K.; Rendell, A.; Burant, J. C.; Iyengar, S. S.; Tomasi, J.; Cossi, M.; Rega, N.; Millam, J. M.; Klene, M.; Knox, J. E.; Cross, J. B.; Bakken, V.; Adamo, C.; Jaramillo, J.; Gomperts, R.; Stratmann, R. E.; Yazyev, O.; Austin, A. J.; Cammi, R.; Pomelli, C.; Ochterski, J. W.; Martin, R. L.; Morokuma, K.; Zakrzewski, V. G.; Voth, G. A.; Salvador, P.; Dannenberg, J. J.; Dapprich, S.; Daniels, A. D.; Farkas, O.; Foresman, J. B.; Ortiz, J. V.; Cioslowski, J.; Fox, D. J. *Gaussian 09* (Revision A.02); Gaussian Inc.: Wallingford, CT, 2009.