Geometry-dependent penetration fields of superconducting Bi$_2$Sr$_2$CaCu$_2$O$_{8+\delta}$ platelets

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Magneto-optical imaging has been used to study vortex penetration into regular polygon-shaped Bi$_2$Sr$_2$CaCu$_2$O$_{8+\delta}$ platelets with various geometries (disks, pentagons, squares, and triangles) but known fixed areas. In all cases we observe an exponential dependence of the field of first penetration, $H_p$, on temperature, consistent with a dominant Bean-Livingston barrier for pancake vortices at our measurement temperatures (45 K – 80 K). However, the penetration field consistently decreases with decreasing degree of sample symmetry, in stark contrast to conventional estimates of demagnetization factors using equivalent ellipsoids based on inscribed circles, which predict the reverse trend. Surprisingly, this observation does not appear to have been reported in the literature before. We demonstrate empirically that estimates using equivalent ellipsoids based on circumscribed circles predict the correct qualitative experimental trend in $H_p$. Our work has important implications for the estimation of appropriate effective demagnetization factors for flux penetration into arbitrarily shaped superconducting bodies.

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I. INTRODUCTION

The Meissner phase in type-II superconductors is separated from the mixed state by the lower critical field, $H_{c1}$. Above $H_{c1}$, the presence of flux in the form of quantized vortices becomes energetically favorable. However, as the magnetic field at the sample edges approaches $H_{c1}$ and vortices begin to nucleate, several energy barriers prevent their penetration into the bulk of the superconductor until the field at the edge is increased to the penetration field $H_p$, where $H_p > H_{c1}$. An additional complication is the existence of large demagnetization factors, dependent on sample size and shape, which enhance the local field at the sample edges and reduce the value of the applied field where first penetration occurs. These enhancement factors can be very difficult to estimate accurately for general sample shapes. The possible penetration of flux inside a superconducting sample and the associated resistive losses experienced when a current is applied represent serious problems for applications of superconductivity. Hence it is vital to develop a complete understanding of surface barriers and more accurate models of demagnetization effects in various sample geometries to be able to extend the range of the flux-free state.

II. EXPERIMENTAL METHOD

Microfabricated structures on the surface of Bi$_2$Sr$_2$CaCu$_2$O$_{8+\delta}$ (BSCCO) single crystals have been shown to be model systems for investigating surface barriers (Bean-Livingston and geometrical) to flux penetration. Previous works have focused on investigations of the temperature dependence of penetration into circular disks of various sizes. Here we describe an extension of these studies to look at the role that the sample geometry plays in the vortex penetration process. We have fabricated arrays of BSCCO disks, pentagons, squares, and triangles of fixed known area and measured their temperature-dependent penetration fields $H_p(T)$ using differential magneto-optic imaging (MOI). In the regime studied $H_p(T)$ was observed to decay exponentially with temperature and, in stark conflict with conventional estimates of the demagnetization factors, falls with the decreasing degree of symmetry of the sample.

Single crystals of BSCCO ($T_c \approx 92 K$) were grown using the floating zone method. Arrays of shallow pillars with the four different symmetries were etched into the surface of freshly cleaved crystals using optical lithography and argon ion-milling techniques. Optical micrographs of typical sample arrays are shown in Fig. 1. In each case, structures of different area are patterned at the corners of a repeating 40 µm square cell and the pillar height is 300 nm. The four sizes of the circular disks (A1-A4) have diameters: 20, 15, 10 and 5 µm and the dimensions of the other regular polygons have been designed to conserve these four areas (c.f., Table I).

We assume that the influence of the underlying optimally doped BSCCO platelet on $H_p(T)$ is negligible due to the substantial suppression of bulk pinning in our measurement temperature range (45 K – 80 K).
Magneto-optical imaging (MOI) has previously been shown to be a very useful technique for studying flux penetration into BSCCO mesostructures. A schematic of the experimental setup is shown in Fig 2. The technique exploits the magneto-optic Faraday effect: the rotation of the plane of polarization of light in the presence of a magnetic field. Key to the emergence of MOI as a tool for detecting stray fields on mesoscopic superconductors was the development of ferrimagnetic garnet films with in-plane anisotropy, which greatly enhance the sensitivity of the system. In this instance, a Bi-doped yttrium iron garnet film was pressed into intimate contact with the sample using screws. The whole assembly was then attached to the cold head of a cryocooler for imaging experiments. Further details of the garnet and the entire measurement system can be found in the literature.

### III. EXPERIMENTAL RESULTS

Several experimental and theoretical studies have established the Bean-Livingston barrier as the dominant barrier for pancake vortices in BSCCO at $T > 15K$. Theory predicts $H_p(T)$ will take the form:

$$H_p = P \frac{\sqrt{2} \kappa}{\ln \kappa} H_c(0) \left[ 1 - \left( \frac{T}{T_c} \right)^2 \right] e^{-T/T_n}, \quad (1)$$

where $\kappa$ is the Ginzburg-Landau parameter, $P$ is the inverse field enhancement factor and $T_n$ is a characteristic temperature for the penetration process. For ease of comparison with Eq. (1), Figs. 4 and 5 display experimental data in the form $\ln[H_p(T)/(1-(T/T_c)^2)]$ versus $T$. Figure 4 displays penetration field data for the largest sized shape (A1) of each geometry in the temperature range 45 K – 75 K. Linear fits based on Eq. (1) have been plotted (choosing $T_n = 34K$ and $T_c = 92K$), and are in excellent agreement with our data, confirming the exponential temperature dependence predicted by Eq. (1). The prefactors $[(P\sqrt{2}/\ln \kappa)H_c(0)]$ extracted from these fits are discussed later, as they contain information regarding the surface field enhancement and quantify the trend that is clearly observed in Fig. 4. $H_p$ falls systematically with decreasing sample symmetry for a given sample area.
Fig 4. (Color online) $\ln[H_p(T)/(1-(T/T_c)^2)]$ versus $T$ for the largest BSCCO mesostructures (A1). Data points are experimental data; dashed lines are fits to Eq. (1) with $T_o = 34K$ and $T_c = 92K$.

MOI spatial resolution is limited by the finite sample/garnet spacing, and accurate sample preparation was paramount in achieving high resolution. This, combined with cryocooler vibrations of the order of ~1µm made it impossible to resolve penetration of flux into the smallest A4 structures in all cases. A2 and A3 exhibit the same trend as the A1 structures shown in Fig. 4, with again providing an excellent description using fits based on Eq. (1). To illustrate this point, Fig. 5 plots the temperature dependence of the penetration field for the three largest square structures, each of which is seen to exhibit the same exponential temperature dependence with a different size-dependent prefactor.

Analytical solutions for demagnetization factors exist only for ellipsoidal-shaped magnetic bodies. As a consequence, demagnetization effects in arbitrarily shaped superconducting bodies are commonly approximated by those for “equivalent” ellipsoids. For an ellipsoid with a magnetic field $H_e$ applied parallel to one of the principal axes, the effective magnetic field ($H_{eff}$) at the equator is

$$H_{eff} = \frac{H_e}{1-D^2}.$$  

where $D$ is the demagnetisation factor which can take values between 0 and 1, and the inverse enhancement factor in Eq. (1) is $P = (1-D)$. For an oblate ellipsoid with principal axes $(a, a, c)$ along $(x, y, z)$ directions and with the field applied along $z$ it can be shown that

$$D = \frac{1}{e} \left( e - \sqrt{1 - e^2 \sin^2 e} \right),$$

where $e = (1-c^2/a^2)^{1/2}$. Expanding (3) to second order in $c/a$ yields

$$P = (1-D) \approx \frac{\pi}{2} \frac{c}{a} - 2 \frac{c^2}{a^2}.$$  

One might expect that a good approximation to the field at the edge of a disk of radius $R$ and thickness $d << R$ in a perpendicular field $H_e$ could be obtained by replacing the disk by an oblate ellipsoid with major axis $b = R$ and minor axis $c = d/2$. Combining (2) and (4) (ignoring the second-order term) would yield the result for the field at the edge $H_{eff} = H_e/(2a/\pi c) = H_e(4R/\pi d) \approx H_e(R/d)$. However, Geshkenbein and Larkin\textsuperscript{12} suggested that a better approximation corresponds to a different choice of elliptical cross section with a larger semi-minor axis, such that the radius of curvature at the edge is approximately $d/2$.\textsuperscript{12} (The radius of curvature of an oblate ellipsoid at $(x, y, z) = (a, 0, 0)$ is $r(a, 0, 0) = c^2/a$.) Zeldov et al.\textsuperscript{13} have demonstrated that this leads to a more accurate value of $H_{eff} \approx H_e(R/d)^{3/2}$ in the limit $\lambda < d << R$, a result which was confirmed by experiments on mesoscopic BSCCO structures\textsuperscript{14-15} and our own observations here. The same approach has been used to estimate the penetration field in long strips and disks.\textsuperscript{14-15} Figure 6 shows the applied field at penetration plotted against the inverse quarter power of the sample area, $A^{-1/4}$. Since the areas (A1-A3) are proportional to the radius of the equivalent disks squared, the good linear fits are consistent with the expected functional relationship of $H_p \propto R^{-3/2}$. A more critical analysis of Fig. 6 reveals that, while the data for the triangular samples extrapolates to a point near the
As expected from Eq. (1), the data for squares and disks extrapolate to significant positive intercepts (9 Oe and 17 Oe respectively). Since penetration must surely occur at H=0 for an infinite platelet this suggests that these data points in Fig. 6 would be better described by a sublinear relationship that passes close to the origin. This apparent discrepancy may be due to the fact that we are not strongly in the limit described in reference 13 since d ~ λ in our samples. It is interesting to note that plots of similar data for somewhat thicker BSCCO disks and squares in reference 4 actually exhibit negative intercepts at \((d/R)^{1/4} = 0.4\).

![Graph showing 3D microstructures](Image)

**Fig. 6.** (Color online) \(H_p\) versus \(a^{1/4}\) for disk-shaped, square, and triangular BSCCO mesostructures at \(T = 55K\). The smallest structures (A4) and the A3 pentagons were beyond the resolution of this experiment.

Theoretical fits to our experimental measurements based on Eq. (1) using \(T_c = 34K\) yield the values for the prefactor \([P\sqrt{2\kappa/\ln\kappa}H_{ci}(0)]\) recorded in Table II. These are in reasonably good agreement with other similar measurements in the literature.\(^{3,4}\) Taking \(\kappa \approx 100\) and \(H_{ci}(0) \approx 100\) Oe,\(^{3,16}\) we can then estimate the values for the inverse enhancement factor \(P\) for each geometry and size.

The demagnetization factors of polyhedra have commonly been approximated by inscribed ellipsoids of revolution.\(^{15}\) In our case, and imposing the above condition on the radius of curvature at the edge, \(c^2/a = d/2\), this corresponds to a choice of \(a = b = r_c\), \(c = (r_c/d)^{1/2}\) and (from Eqn. 4) \(P(n) \equiv (\pi^2/8r_c)^{1/2}\), where \(r_c\) is the inscribed radius of a regular polygon with \(n\)-fold rotational symmetry (the subscript \(i\) denotes use of an inscribed circle). However, noting that the radii of inscribed circles \(r_c\) vary as \(r_c(\text{tri}) < r_c(\text{sqa}) < r_c(\text{pent}) < r_c(\text{disk})\), it is clear that this approach gives \(H_p(\text{tri}) > H_p(\text{sqa}) > H_p(\text{pent}) > H_p(\text{disk})\). The experimentally measured field enhancement parameters \((P_{exp})\) are listed alongside these theoretical estimates \((P_i)\) in Table II and it is clear that the trend of the predictions for inscribed ellipsoids are in direct contradiction with our experimental observations. We note that the penetration fields of similar freestanding BSCCO microstructures (circular disks and squares) were also compared in Ref. 4. Although the authors did not comment on it in that paper, and data were not presented at directly comparable temperatures for the two shapes, their penetration fields for squares also appear to be significantly lower than circular disks of the same width and thickness for \(T \geq 45K\).

**IV. DISCUSSION**

Many theoretical studies have been devoted to the calculation of demagnetization factors for magnetic bodies with a range of regular shapes. Much of this work has arisen in the context of ferromagnetism where accurate demagnetization factors are vital for the precise calculation of magnetostatic energies. Since demagnetization fields are not uniform in arbitrarily shaped bodies, such calculations yield effective average values; for example, the magnetometric demagnetizing factor of an arbitrary sample in the \(z\)-direction, \(D_z\), can be defined as the factor that makes the magnetostatic self-energy per unit volume equal to \(2\pi D_z M_s^2\), where \(M_s\) is its saturation magnetization. A comparison with estimates based on values obtained from equivalent ellipsoids is frequently made. For example, Aharoni presents analytical results for the demagnetization factors of rectangular ferromagnetic prisms and notes very significant discrepancies from values obtained for a prolate spheroid with the same aspect ratio.\(^{18}\) To address this issue, Beleggia et al.\(^{19}\) have calculated the equivalent ellipsoid for uniformly magnetized disks, cylinders with elliptical cross-section and prisms, by imposing equality between the demagnetization factors of the two shapes of equal volume. Demagnetization factors have also been calculated for magnetic materials under other assumptions, e.g., for a fixed value of the magnetic susceptibility, \(\chi\). Making an explicit connection to the Meissner state in superconductors, Pardo et al.\(^{20}\) and Chen et al.\(^{21}\) have numerically calculated the magnetometric demagnetization factors for perfectly diamagnetic (\(\chi = -1\)) square prisms and cylinders. In practice, however, penetration in our pillars occurs at the point on the surface where the effective field (demagnetizing field) is highest, and these average calculations are of little practical use. Moreover, none of these works accounts for the penetration of flux lines in a realistic way; for example, the field lines at the edges do not have the expected curvature as discussed above.\(^{12}\)

Berdiyorov et al.\(^{22}\) describe a theoretical study that addresses a situation much closer to the one found in our experiments. They have calculated numerical solutions to the non-linear Ginzburg-Landau equations for vortex penetration into mesoscopic superconducting disks, rings, and squares. They find that the Bean-Livingston energy barrier that has to be overcome for a single vortex to enter a sample is lower at the middle of one edge of a square.
than on the circumference of a disk of the same width and thickness. Hence first flux penetration occurs at significantly lower fields in the square, in apparent agreement with our experimental observations. We note, however, that these calculations have been made for samples with \( r = 4 \xi, \quad d = 0.1 \xi, \quad \kappa = 1 \) and so are in a very different regime from our samples with \( r \gg \xi, \quad d \gg \xi, \quad \kappa \approx 100 \).

Finally we make the empirical observation that the qualitative trend exhibited by our experimental data is captured if we base equivalent ellipsoids on the radius of the circumscribed circle instead of the inscribed circle considered above. The radius, \( R_n \), of a circumscribed circle surrounding an \( n \)-sided regular polygon with side of length \( S_n \) is

\[
R_n = \frac{S_n}{2 \sin \left( \frac{\pi}{n} \right)}.
\]

(5)

Choosing \( a = b = R_n \), and \( c = (R_n d / 2)^{1/2} \), theoretical values of \( P_i(n) \) (the subscript c denotes use of a circumscribed circle) for our BSCCO platelets have been generated by combining Eqs. (4) and (5) and are displayed in Table II. Comparing experimental data with the circumscribed circle model, we note that the trend with decreasing degree of symmetry is now correct. However, a comparison of columns \( P_{exp}/P_{ref} \) and \( P_i(n)/P_{c,ref} \), where the inverse enhancement factors have been normalized by that of a reference disk of area \( A_1 \), reveals that the theoretical predictions do consistently overestimate the observed values. Aside from these numerical differences, we believe that this is the first time that it has been pointed out that equivalent ellipsoids based on circumscribed rather than inscribed circles yield a qualitatively better estimate of the trend in demagnetization factors as a function of degree of symmetry in polygon-shaped superconducting platelets. Our observations have rather important implications for the estimation of appropriate effective demagnetization factors for flux penetration into arbitrarily shaped superconducting bodies. In particular, it is surprising that the experimental field enhancement factor for the triangular platelets is so much larger than the other structures. Clearly a model based on circumscribed circles is too simple to capture all the physics of the problem of flux penetration which must also consider the distribution of supercurrent densities and the role of sharp/rounded corners etc. Hence we hope that this paper will stimulate new theoretical work to fully understand this.

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\begin{array}{|c|c|c|c|c|c|c|c|}
\hline
\text{Mesoscopic Structure} & \text{Prefactor (Oe)} & P_{exp} & P_{exp}/P_{ref} & P_i(n) & P_i(n)/P_{c,ref} & P_c(n) & P_c(n)/P_{c,ref} \\
\hline
A1 & - Disk & 270 \pm 5 & 0.0893 \pm 0.0016 & 1.000 & 0.166 & 1.000 & 0.166 & 1.000 \\
& - Pentagon & 236 \pm 5 & 0.0787 \pm 0.0018 & 0.882 & 0.172 & 1.032 & 0.157 & 0.942 \\
& - Square & 211 \pm 3 & 0.0699 \pm 0.0010 & 0.783 & 0.175 & 1.054 & 0.151 & 0.907 \\
& - Triangle & 134 \pm 3 & 0.0446 \pm 0.0010 & 0.500 & 0.185 & 1.112 & 0.137 & 0.823 \\
A2 & - Disk & 306 \pm 15 & 0.1053 \pm 0.0053 & 1.179 & 0.188 & 1.131 & 0.188 & 1.131 \\
& - Square & 262 \pm 7 & 0.0877 \pm 0.0022 & 0.983 & 0.198 & 1.189 & 0.171 & 1.027 \\
A3 & - Square & 329 \pm 18 & 0.1136 \pm 0.0061 & 1.273 & 0.233 & 1.402 & 0.202 & 1.217 \\
\hline
\end{array}
\]

TABLE II. Experimentally and theoretically derived inverse enhancement factors \( P \) for various BSCCO mesostructures. The areas of the \( n \)-sided regular polyhedra A1-A3 are contained in Table I. \( P_i(n) \) and \( P_c(n) \) are theoretically derived using the methods of inscribed and circumscribed ellipsoids respectively. \( P_{exp} \), \( P_{ref} \), \( P_{c,ref} \) are the experimental and theoretical values of \( P \) for the A1 disk structure. The height of mesoscopic pillars is 300 nm in all cases.


V. B. Geshkenbein and A. I. Larkin (private communication).


